

Thermal Transient Computational Information

Software Version 3.2

1. Acquired Data

Symbol	Description
V_n	acquired voltage samples, sampled and quantized $V(t)$
I_n	acquired current samples, sampled and quantized $I(t)$
t_n	acquired sample times

2. Thermal Transient Computation

Symbol/Equation	Description
$R_n = V_n/I_n$	sampled bridgewire resistance
$V_{\text{corr}_n} = R_n * I_{\text{test}}$	corrected voltage, I_{test} = requested test current
$P_{VA}(), P_{IA}(), P_{RA}()$	regression predictors for $V(t)$, $I(t)$ and $R(t)$ computed over $R_A = [t_A, t_A + \Delta t_A]$
$P_{VB}(), P_{IB}(), P_{RB}()$	regression predictors for $V(t)$, $I(t)$ and $R(t)$ computed over $R_B = [t_{\text{pulse}} - t_B - \Delta t_B, t_{\text{pulse}} - t_B]$
$V_{\text{TR}} = P_{VB}(t_{\text{pulse}}) - P_{VA}(t_{\text{TR}})$	Thermal Response voltage
$R_0 = P_{RA}(t_{\text{start}})$	initial (cold) resistance
$\Delta R = P_{RB}(t_{\text{pulse}}) - P_{RA}(t_{\text{start}})$	total change resistance. Note that the ΔR change in resistance does not correspond to the V_{TR} change in voltage.
$P_{RA}^{-1}()$	inverse function of P_{RA} predictor
$\tau = P_{RA}^{-1}(P_{RB}(t_{\text{pulse}}))$	thermal response time constant

Note: $t_A, \Delta t_A, t_B, \Delta t_B, t_{\text{TR}}$ are programmable values. Please refer to Figure A.

Default settings:

$t_A = 72.5\mu\text{S}$	$\Delta t_A = 145\mu\text{S}$	$t_{\text{TR}} = 100\mu\text{S}$
$t_B = 0\mu\text{S}$	$\Delta t_B = 362.5\mu\text{S}$	

3. Heat Model Analysis

Symbol/Equation	Description
α_{BW}	bridgewire temperature resistance coefficient
$\Theta = \frac{1}{\alpha_{BW}} \cdot \frac{\Delta R}{R_0}$	final bridgewire temperature offset from ambient
$\overline{PA} = [P_{IA}(t_{\text{AMID}})]^2 \cdot P_{RA}(t_{\text{AMID}})$	average dissipated power over range R_A
Slope(P_{RA}), Slope(P_{RB})	P_{RA} and P_{RB} predictor slopes

(continued on next page)

$$C_p = \frac{E_A}{\Delta T_A} = \frac{\overline{P_A} \cdot \Delta t_A}{\frac{\Delta R_A}{R_0} \cdot \frac{1}{\alpha_{BW}}} = \overline{P_A} \cdot R_0 \cdot \alpha_{BW} \cdot \frac{\Delta t_A}{\Delta R_A} = \alpha_{BW} \frac{\overline{P_A} \cdot R_0}{\text{Slope}(P_{RA})}$$

C_p of the bridgewire

$$\overline{P_B} = \frac{E_B}{\Delta t_B} = \frac{C_p \Delta T_B}{\Delta t_B} = CP \frac{1}{\Delta t_B} \cdot \frac{\Delta R_B}{R_0} = \frac{C_p}{\alpha_{BW} \cdot R_0} \text{Slope}(P_{RB})$$

average dissipated power over range R_A

$$\gamma = \frac{\overline{P_A} - \overline{P_B}}{\Theta} \quad \text{thermal conductance in } \left[\frac{\text{Watts}}{\text{deg C}} \right]$$

$$IF_n, \quad \left(\frac{dIF}{dt} \right)_n \quad \text{filtered } I_n \text{ and } \left(\frac{dI_n}{dt} \right)_n, \text{ respectively}$$

$$RF_n, \quad \left(\frac{dRF}{dt} \right)_n \quad \text{filtered } R_n \text{ and } \left(\frac{dR_n}{dt} \right)_n, \text{ respectively}$$

$$T_n = \left(\frac{RF_n}{R_0} - 1 \right) \cdot \frac{1}{\alpha_{BW}} \quad \left(\frac{dT}{dt} \right)_n = \frac{\left(\frac{dRF_n}{dt} \right)_n}{R_0} \cdot \frac{1}{\alpha_{BW}}$$

bridgewire temperature

$$P_n = IF_n^2 \cdot RF_n \quad \text{total dissipated power}$$

$$C_{p_n} = \frac{E_n}{\Delta T_n} = \frac{P_n}{\frac{\Delta T_n}{\Delta t_n}} = \left(\frac{dT}{dt} \right)_n \quad \text{instant } C_p \text{ of the bridgewire}$$

$$P_{BW_n} = \frac{E_{BW_n}}{\Delta T_n} = \frac{C_{p_n} \cdot \Delta T_n}{\Delta T_n} = C_{p_n} \cdot \left(\frac{dT}{dt_n} \right)_n \quad \text{power consumed on heating the bridgewire proper}$$

$$P_{PH_n} = P_n - P_{BW_n} \quad \text{power dissipated into the rest of the structures}$$

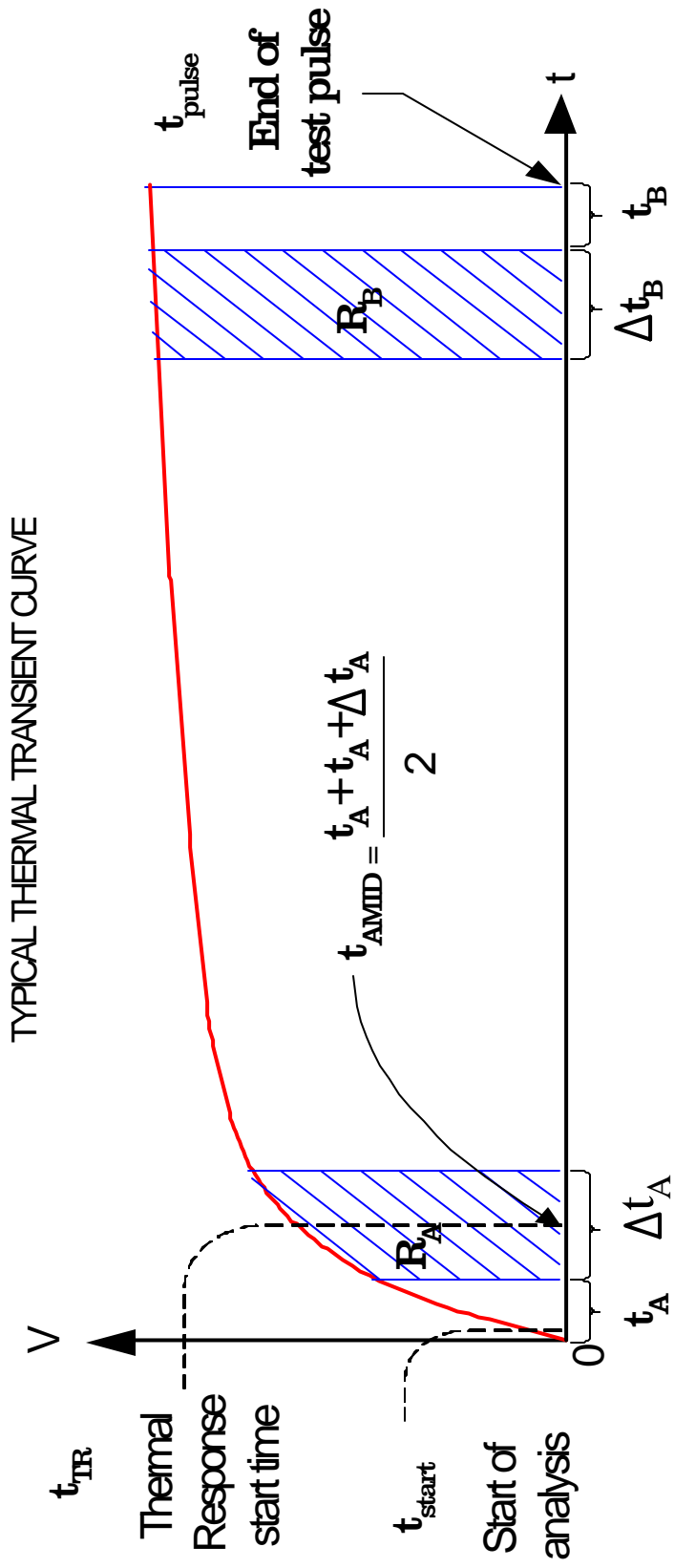


Figure A. Thermal Response Curve Timing